

Apéndice G

Formulario para la Parte I

Estequiometría:

$$n_j = n_{j0} + \frac{\nu_j}{-\nu_i} \cdot (n_{i0} - n_i) \quad (1.2)$$

$$n_{rl} = n_{rl0}(1 - f_{rl}) \quad (1.5)$$

$$n_j = n_{j0} + \frac{\nu_j}{-\nu_{rl}} \cdot n_{rl0} f_{rl} \quad (1.6)$$

$$n_i = n_{i0} + \nu_i \xi \quad (1.8)$$

$$n_T = n_{T0} + \frac{\Delta\nu}{-\nu_{rl}} (n_{rl0} - n_{rl}) \quad (1.14)$$

$$= n_{T0} + \frac{\Delta\nu}{-\nu_{rl}} n_{rl0} f_{rl}$$

$$n_i = n_{i0} + \sum_{r=1}^{n_{rxn}} \nu_{ir} \xi_r \quad (1.19)$$

$$\xi_r = \frac{n_{i0} f_{ir}}{(-\nu_{ir})} \quad (1.23)$$

$$-\sum \nu_{ir} \xi_r = n_{i0} f_i \quad (1.24)$$

$$n_T = n_{T0} + \sum \Delta\nu_r \xi_r \quad (1.26)$$

NOTA: En las ecuaciones anteriores se puede sustituir; n por C para líquidos (ξ por ξ^*); y n por F para gases (ξ por ξ').

Equilibrio:

$$K_C = \frac{C_R^r C_S^s \dots}{C_A^a C_B^b \dots} \quad (2.10)$$

$$K_P = \frac{p_R^r p_S^s \dots}{p_A^a p_B^b \dots} \quad (2.9)$$

Para SOLUCIÓN NUMÉRICA, **modificar** Ecs. 2.10 y 2.9

$$\ln K \equiv \frac{-\Delta G}{R_g T} \quad (2.5)$$

Ec. de van 't Hoff (ΔH -cte y por mol de rxn):

$$K_P \simeq K_{P_{ref}} e^{\frac{-\Delta H_{cte}}{R_g} \left(\frac{1}{T} - \frac{1}{T_{ref}} \right)} \quad (2.17)$$

Cinética (1 rxn):

$$\mathbf{r}_i \equiv \frac{1}{V} \frac{dn_i}{dt} \quad (3.1)$$

$$\mathbf{r} \equiv \frac{1}{\nu_i} \frac{1}{V} \frac{dn_i}{dt} = \frac{1}{V} \frac{d\xi}{dt} \quad (3.5 \text{ y } 3.6)$$

$$\mathbf{r}_i = \nu_i \mathbf{r} \quad (3.19)$$

Relacionar velocidades (r es reacción; i y j componentes):

$$\mathbf{r}_i = \sum_{r=1}^{n_{rxn}} \mathbf{r}_{ir} \quad (4.20)$$

$$\mathbf{r}_{jr} = \frac{\nu_{jr}}{\nu_{ir}} \mathbf{r}_{ir} \quad (4.22)$$

$$\mathbf{r}_i = \sum_{r=1}^{n_{rxn}} \nu_{ir} \mathbf{r}_r \quad (4.23)$$

Ec. de Arrhenius:

$$k = A e^{\frac{-E_A}{R_g T}} \quad (3.22)$$

Tiempo Espacial:

$$\tau \equiv \frac{V_R}{\dot{V}_0} \quad (4.1)$$

Tiempo de Residencia (R. Continuos):

$$t_1 = \int_0^{V_{R1}} \frac{dV_R}{\dot{V}} \quad (4.2)$$

Relación Flujo-Concentración:

$$F_i = \dot{V} C_i$$

ECUACIONES DE DISEÑO

R. por Lotes (para V_{R1} -cte):

$$t_1 = C_{rl0} \int_0^{f_{rl1}} \frac{df_{rl}}{(-r_{rl})} \quad (4.7)$$

$$\frac{df_{rl}}{dt} = \frac{(-r_{rl})}{C_{rl0}} \quad (7.16)$$

$$\frac{dC_i}{dt} = \mathbf{r}_i \quad (4.8)$$

Si V_{R1} -variable [P_{CTE}]:

$$t_1 = C_{rl0} \int_0^{f_{rl1}} \frac{df_{rl}}{(-r_{rl})(1 + \delta_{rl} f_{rl}) \left(\frac{T}{T_0} \right)}$$

R. de Tanque Agitado (k reactores en serie), $\tau_k = \frac{V_{Rk}}{\dot{V}_0}$:

$$\tau_k = \frac{V_{Rk}}{\dot{V}_0} = \frac{C_{rl0} (f_{rlk} - f_{rlk-1})}{(-r_{rl})_k} \quad (4.11)$$

$$V_{Rk} = \frac{F_{ik} - F_{ik-1}}{(\mathbf{r}_i)_k} \quad (4.12)$$

Para líquidos (varias rxnes):

$$\tau_k = \frac{V_{Rk}}{\dot{V}_0} = \frac{C_{ik} - C_{ik-1}}{(\mathbf{r}_i)_k} \quad (4.13)$$

Para SOLUCIÓN NUMÉRICA, **modificar** Ecs.4.11, 4.12 y 4.13

$$[\mathbf{A} - \mathbf{B}] \times 10^0 = 0$$

R. de Flujo Pistón:

$$\tau_{1l} = C_{rl0} \int_0^{f_{rl1}} \frac{df_{rl}}{(-r_{rl})} \quad (4.17)$$

$$\frac{df_{rl}}{d\tau} = \frac{(-r_{rl})}{C_{rl0}} \quad (7.39)$$

$$\frac{dF_i}{dV_R} = r_i \quad (4.18)$$

Para líquidos (varias rxnes):

$$\frac{dC_i}{d\tau} = r_i \quad (4.19)$$

Para gases ideales:

$$\delta_{rl} = \frac{y_{rl0} \Delta\nu}{-\nu_{rl}} \quad (6.9)$$

$$\dot{V} = \dot{V}_0 (1 + \delta_{rl} f_{rl}) \left(\frac{T}{T_0} \right) \left(\frac{P_{T0}}{P_T} \right) \quad (6.12)$$

$$\dot{V} = \dot{V}_0 \left(\frac{\sum F_i}{\sum F_{i0}} \right) \left(\frac{T}{T_0} \right) \left(\frac{P_{T0}}{P_T} \right) \quad (6.11)$$

$$C_i = \left(\frac{C_{i0} + \frac{\nu_i}{(-\nu_{rl})} C_{rl0} f_{rl}}{1 + \delta_{rl} f_{rl}} \right) \left(\frac{T_0}{T} \right) \left(\frac{P_T}{P_{T0}} \right) \quad (6.19)$$

$$C_i = \left(\frac{F_i}{F_T} \right) C_T = \left(\frac{F_i}{F_T} \right) \frac{P_T}{R_g T} \quad (6.20)$$

Calor de Reacción de referido a ...

$$\Delta H_{jr} = \Delta H_{ir} \frac{|\nu_{ir}|}{|\nu_{jr}|} = \frac{\Delta H_r}{|\nu_{jr}|} \quad (7.1)$$

NOTA: En las ecuaciones que se presenta a continuación si aparece r_l se refiere a una reacción; si aparece F_i se refiere a gases mientras que si aparece ρ a líquidos.

OPERACIÓN ADIABÁTICA (sólo si propiedades constantes):

$$T = T_0 - \frac{\Delta H_{rl} C_{rl0} f_{rl}}{\rho C_P} \Rightarrow T = T_0 + m f_{rl} \quad (7.5)$$

$$T = T_0 - \frac{\Delta H_{rl} F_{rl0} f_{rl}}{\sum F_i C_{Pi}} \Rightarrow T = T_0 + \frac{f_{rl}}{b + m f_{rl}} \quad (7.6)$$

$$T = T_0 - \frac{\sum_{r=1}^{n_{rxn}} \Delta H_r \xi_r^*}{\rho C_P} \Rightarrow T = b + \sum_{\text{indep}} m_i C_i \quad (7.7)$$

$$T = T_0 - \frac{\sum_{r=1}^{n_{rxn}} \Delta H_r \xi_r'}{\sum F_i C_{Pi}} \Rightarrow T = b + \frac{\sum_{\text{indep}} m_i F_i}{b_2 + \sum_{\text{indep}} m_{2i} F_i}$$

OPERACIÓN CON INTERCAMBIO

Reactor por Lotes:

$$\frac{dT}{dt} = \frac{\dot{Q}_{tr}}{V_{R1} \rho C_P} - \frac{\Delta H_{rl} (-r_{rl})}{\rho C_P} \quad (7.15)$$

$$\frac{dT}{dt} = \frac{\dot{Q}_{tr}}{V_{R1} \rho C_P} - \sum_{r=1}^{n_{rxn}} \frac{\Delta H_r r_r}{\rho C_P} \quad (7.13)$$

Si T_C es constante (Lotes y Tanque):

$$\dot{Q}_{tr} = UA (T_C^{sat} - T) \quad (7.17)$$

$$= \dot{m}_{cond} \lambda_{vap} \quad \text{si } T_C^{sat} > T \quad (7.18)$$

$$= -\dot{m}_{evap} \lambda_{vap} \quad \text{si } T_C^{sat} < T \quad (7.19)$$

Si T_C cambia (Lotes y Tanque):

$$\dot{Q}_{tr} = -\dot{V}_C \rho C_P C_{PC} (T_{C1} - T_{C0}) \quad (7.21 \text{ y } 7.22)$$

$$= \dot{V}_C \rho C_P C_{PC} (T_{C0} - T) \left(1 - e^{-\frac{UA}{\dot{V}_C \rho C_P C_{PC}}} \right)$$

Reactores de Tanque Agitado (7.26 a 7.29):

$$\dot{V}_0 \rho C_P (T_k - T_{k-1}) = \dot{Q}_{trk} - \Delta H_{rl} \dot{V}_0 C_{rl0} (f_{rlk} - f_{rlk-1})$$

$$T_k = \frac{UA T_{Ck} + \dot{V}_0 \rho C_P T_{k-1} - \Delta H_{rl} \dot{V}_0 C_{rl0} (f_{rlk} - f_{rlk-1})}{\dot{V}_0 \rho C_P + UA}$$

$$\dot{V}_0 \rho C_P (T_k - T_{k-1}) = \dot{Q}_{trk} - \sum_{r=1}^{n_{rxn}} \Delta H_r (\xi'_{rk} - \xi'_{rk-1})$$

$$T_k = \frac{UA T_{Ck} + \dot{V}_0 \rho C_P T_{k-1} - \sum_{r=1}^{n_{rxn}} \Delta H_r (\xi'_{rk} - \xi'_{rk-1})}{\dot{V}_0 \rho C_P + UA}$$

Reactores Tubulares:

$$\frac{dT}{d\tau} = \frac{\frac{4}{D} U (T_C - T) - \Delta H_{rl} (-r_{rl})}{\rho C_P} \quad (7.37)$$

$$\frac{dT}{d\tau} = \frac{\frac{4}{D} \dot{V}_0 U (T_C - T) - \dot{V}_0 \Delta H_{rl} (-r_{rl})}{\sum F_i C_{Pi}} \quad (7.38)$$

$$\frac{dT}{d\tau} = \frac{\frac{4}{D} U (T_C - T) - \sum_{r=1}^{n_{rxn}} \Delta H_r r_r}{\rho C_P} \quad (7.40)$$

$$\frac{dT}{dV_R} = \frac{\frac{4}{D} U (T_C - T) - \sum_{r=1}^{n_{rxn}} \Delta H_r r_r}{\sum F_i C_{Pi}} \quad (7.41)$$

$$\frac{dT_C}{dV_R} = \begin{cases} -\frac{\frac{4}{D} U (T_C - T)}{F_C C_{PC}} & \text{concurrente.} \\ +\frac{\frac{4}{D} U (T_C - T)}{F_C C_{PC}} & \text{contracorriente.} \end{cases} \quad (7.45)$$

Si calentamiento uniforme: $\frac{4}{D} U (T_C - T) \Rightarrow \frac{\dot{Q}_{tr}}{V_{R1}}$
Si se requiere en Ec. 7.45: $dV_R \Rightarrow \dot{V}_0 d\tau$ y/o $F_C \Rightarrow V_C \rho C$

ABC para comprender Reactores con Multireacción. Segunda Edición.

ISBN 978-607-29-3556-3 publicado el 7 de julio de 2022.

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